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(54) Title: PULSE SHAPING SIGNALS FOR ULTRAWIDEBAND COMMUNICATION
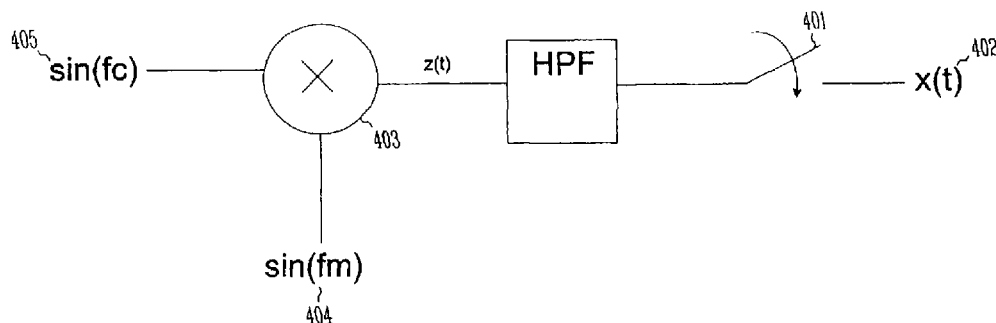
(57) Abstract: An ultrawideband radio frequency pulse is generated by shaping a carrier signal having a selected frequency with a window function. The shaped carrier is gated to produce the ultrawideband pulse. In further embodiments, the window function comprises a sinusoidal function, and the ultrawideband pulse is formed via a mixer and a CMOS radio frequency switch.

PULSE SHAPING SIGNALS FOR ULTRAWIDEBAND COMMUNICATION

Technical Field

Various embodiments of the invention relate generally to ultrawideband
5   communications, and more specifically to pulse shaping finite duration signals for use in
an ultrawideband communication system.

Background

Electric signals used for wireless communication typically include a carrier signal
10   that exists independent of the data being conveyed, and a modulation signal that is applied
to the carrier signal to embed the conveyed data into the carrier. The modulated carrier
signal is then conveyed as radio frequency electromagnetic waves to a receiver, which
extracts the modulation signal data from the carrier frequency and so recovers the data.

Carrier signals are typically designed to have one or more narrow, carefully
15   controlled frequencies, ensuring that radiated power is controlled to be within specified
guidelines and is used to the greatest benefit of the transmitting device. But, some
systems have adapted wireless communications methods having a seemingly inconsistent
approach, which is to spread the signal frequency out over a very wide range, resulting in
a low fraction of total transmitted power at any one specific frequency. Such signals are
20   often called ultrawideband signals, and are being explored for short-range
communications systems, such as wireless networks, as well as for some special functions
like radar in which the bandwidth makes such a signal difficult to jam. But, generation of
an ultrawideband signal is not a trivial task, and requires methods and circuits different
from those traditionally used to produce narrow carrier signals.

25   A system for producing ultrawideband signals is therefore desired.

Brief Description of the Figures

Figure 1 illustrates a variety of sinusoidal window functions, consistent with
various embodiments of the present invention.

30   Figure 2A shows the modulation product of a window function p(t) applied to a
sinusoidal carrier signal s(t) .

Figure 2B shows a magnified portion of Figure 2, consistent with an embodiment of the present invention.

Figure 3 shows the spectrum of the product of the window function p(t) and the sinusoidal carrier signal s(t), consistent with an embodiment of the present invention.

5   Figure 4 shows a single balance mixer and a CMOS RF switch, consistent with one embodiment of the present invention.

Figure 5 shows cascaded double balanced mixers and a CMOS RF switch, consistent with an embodiment of the present invention.

Figure 6 shows a variable transconductance circuit and CMOS RF switch,

10   consistent with an embodiment of the present invention.

Figure 7 shows a combination of fixed gm amplifiers with a CMOS RF switch, consistent with an embodiment of the present invention.

Figure 8 is a circuit diagram, illustrating construction of an RF switch as is used to gate the window-shaped carrier functions consistent with an embodiment of the present

15   invention.

Figure 9 shows one embodiment of construction of the circuit of Figure 8 using CMOS, consistent with an embodiment of the present invention.

Figure 10 illustrates an ultrawideband data communications system, consistent with an embodiment of the present invention

20

Detailed Description

In the following detailed description of sample embodiments of the invention, reference is made to the accompanying drawings which form a part hereof, and in which is shown by way of illustration specific sample embodiments in which the invention may be

25   practiced. These embodiments are described in sufficient detail to enable those skilled in the art to practice the invention, and it is to be understood that other embodiments may be utilized and that logical, mechanical, electrical, and other changes may be made without departing from the spirit or scope of the present invention. The following detailed description is, therefore, not to be taken in a limiting sense, and the scope of the invention

30   is defined only by the appended claims.

The present invention provides in various embodiments a system for generating ultrawideband radio frequency pulses. A carrier signal having a selected frequency is

generated, and is shaped with a window function to produce the ultrawideband pulse. The produced pulse is in some embodiments gated by a RF switch, which provides a switched mix of the carrier signal and a sinusoidal shaping signal as its output. The shaping signal or window function used is in various embodiments a sinusoidal function, such as a
5   Hamming, Hanning, or Blackman window, as are traditionally used when working with discrete time-sampled digital data in spectral analysis or to produce finite impulse response filters.

Figure 1 illustrates a variety of sinusoidal window functions, consistent with various embodiments of the present invention. The various functions presented here are
10   representative of functions that are applied to a carrier signal in various embodiments of the invention to produce a ultrawideband radio frequency (RF) product signal. Each of the three functions presented are derived from a sinusoidal function, and have a zero value outside their respective periods "M". Although the functions are traditionally used for digital filtering methods, they are implemented as continuous analog functions for
15   purposes of the example embodiments of the present invention described here and so are shown here as continuous functions rather than as a series of discrete points. The window functions p(t) shown here are applied periodically to a carrier signal s(t) function, resulting in a modulated signal such as is shown generally in Figure 2a.

Carriers and modulation methods vary from application to application, and include
20   such well-known methods as analog amplitude modulation of the carrier as is used in AM radio, and analog frequency modulation of the carrier as is used in FM radio. Similar modulation methods exist for digital signals, including amplitude shift keying in which the amplitude is modulated between discrete values, and frequency shift keying in which the frequency is modulated between discrete values. Additional methods, such as phase shift
25   keying in which the phase of the carrier is inverted to represent a digital symbol, are also useful in digital systems. More sophisticated systems employ multiple methods, such as the commonly used quadrature amplitude modulation method which uses four distinct phases and two distinct amplitudes to encode data.

The carrier itself is another matter of concern, and is typically dictated by the
30   application and by Federal Communication Commission (FCC) regulations. The radio spectrum is carefully regulated to ensure that only certain approved products transmit radio frequency signals at certain frequencies, typically at power levels that are carefully

restricted to minimize interference with other products. The designer of an RF communications system is therefore restricted in carrier frequency and power choice by regulations, and must ensure the product does not transmit excessive power at restricted or unintended frequencies as well as at the carrier frequency.

5   The carrier signal is therefore typically designed to have one or more narrow, carefully controlled frequencies, ensuring that radiated power is controlled to be within the specified guidelines and is used to the greatest benefit of the transmitting device. But, some systems have adapted wireless communications methods having a seemingly inconsistent approach, which is to spread the signal frequency out over a very wide range,

10   resulting in a low fraction of transmitted power at any one specific frequency. Such signals are often called ultrawideband signals, and are characterized by having a bandwidth that is greater than 20% of the center frequency, or alternately that have a bandwidth of 500MHz or greater.

          These signals remain compliant with FCC regulations by emitting only a small

15   amount of power at any given frequency, and rely upon a receiver receiving the full ultra-wide bandwidth signal to provide an adequately strong signal to overcome RF noise and other problems. Such systems are therefore being explored for short-range communications systems, such as wireless networks, as well as for some special functions like radar in which the bandwidth makes such a signal difficult to jam. But, generation of

20   an ultrawideband signal is not a trivial task, and requires methods and circuits different from those traditionally used to produce narrow carrier signals. The example embodiments of the invention presented here illustrate various methods of generating such ultrawideband signals.

          Figure 2b illustrates a magnified view of a portion of Figure 2a, showing the result

25   of combining the window signal p(t) with the carrier signal s(t) to produce modulation product p(t)*s(t). The window function p(t) shown here is applied periodically to a carrier signal s(t) over the duration, Tm, and of deterministic phase, resulting in a modulated signal such as is shown in Figures 2a and 2b. The combined product's spectrum is dependent on the carrier frequency and on the window function applied, as is illustrated in

30   Figure 3. The center frequency of 3.5GHz is the frequency of the carrier signal s(t), while the spectrum width of the primary lobe 301 is dependent on the period of the window

function p(t). Further, the amplitude of secondary lobes 302 and 303 is determined largely by the window function p(t) that is selected.

The peak secondary node amplitude can be estimated by knowing the type of window function p(t) that is employed – a simple rectangular window would be expected to produce peak side lobe amplitudes only 13dB down from the main lobe peak amplitude, for example. Because it is desirable in some embodiments of the present invention to limit amplitude of side lobes to increase the proportion of energy radiated within the intended main lobe 301, the functions of Figure 1 are employed in various embodiments. It is expected that a Hanning window's side lobe peak amplitude will be approximately 31 deciBels down in amplitude from the main lobe peak amplitude, while Hamming window side lobes will peak at approximately 41 dB down and Blackman window side lobes will peak approximately 57 dB down.

The width of the main lobe varies with various functions, too, and must be taken into account when selecting a window function for application to a carrier. For example, a rectangular window produces a main lobe of width 4pi/(m+1), where m is the period of the window. Similarly, Hanning and Hamming functions produce a main spectral lobe of width 8pi/m, while a Blackman window produces a somewhat larger main lobe of 12pi/m. Although the Blackman window again appears to be a good choice for ultrawideband signal production given the main lobe width, these are but a few examples of the broad range of window functions that are employed in different embodiments of the invention.

The product of the window function p(t) and the carrier signal s(t) is in some embodiments of the invention further gated by a gating function G(t), such as by an RF switch. The gating function RF switch controls the time duration and spectral occupancy of the product signal, resulting in an output signal of G(t)*p(t)*s(t). The gating function is further specified in some embodiments of the invention to ensure that produced ultrawideband pulses meet applicable standards or spectral profile mask compliance.

Figures 4-9 illustrate various circuit topologies for implementing RF switch gating of an RF product signal p(t)*s(t), consistent with various embodiments of the present invention. Figure 4 shows a single balance mixer with an RF switch 401, used to gate the output signal x(t) shown at 402. The inputs to mixer 403 include carrier signal 404, a sinusoidal signal with frequency f(m), and Hanning window function 405, implemented as a sinusoidal signal having frequency f(c). Although the window function 405 is a sine

function and not the time-limited cosine function used to define the Hanning window in Figure 1, the RF switch gates the output to limit x(t) such that the output signal is only present over the Hanning window period M of the sinusoidal function applied to the mixer at 405. Reexamination of the window definitions for the window functions presented in

5   Figure 1 reveal that Hanning windows can be implemented using a circuit such as that of Figures 4-9, with a single sinusoidal source and minimal further processing such as offset or scaling. The RF switch is used in various other embodiments of the invention to gate a product of sinusoidal signals to implement windowed carrier signals with other sinusoidal functions, such as the Hamming and Blackman windows of Figure 1, but a second

10 sinusoidal source is employed for the Blackman window and further calibration of voltage offset and scaling is performed to produce the defined window functions.

Figure 5 shows an embodiment having cascaded dual mixers 501 and 502, with each mixer mixing the window function sinusoid 503 with carrier signal 504. The inputs to mixer 501 include carrier signal 501 and a product of the window function sinusoid 503

15 and carrier sinusoid 504. The differential response of MOSFET mixers 501 and 502 result in elimination of common mode input components, so that the output is $\sin^2(fm)*\sin(fc)$ rather than the more complex $\sin(fc)+\sin(fm)+\sin(fc)*\sin(fm)$ product of Figure 4's mixer 403. The resulting product is again gated via RF switch 505 to produce the output signal x(t).

20 Figure 6 shows another example of an ultrawideband generation circuit using an RF gating switch 601. Transistor M0 is biased to operate in the constant current region, and transistor M1 is biased to operate in the triode region. The transconductance of M1 can be varied as a function of input carrier signal RF and shaping signal LO, which are further provided to a second complementary circuit such that RF is 180 degrees out of

25 phase but LO remains the same. The output Vout at 604 and the corresponding Vout from the second complementary circuit form a differential output, which is a shaped function of input carrier signal RF. If input signal RF is sin(fm) and input shaping signal LO is sin (fc), the differential output is $\sin^2(fm)*\sin(fc)$, as in the cascaded double balance mixer circuit of Figure 5. In such an embodiment, the RF signal coupled to the gate of M0 at

30 602 corresponds to the sin(fm) signal shown at 504 of Figure 5, and the input shaping signal LO coupled to the gate of M1 at 603 corresponds to the window function sinusoid

illustrated at 503. The circuit of Figure 6 and its complementary circuit form the cascaded double balance mixer shown as 501 and 512 of Figure 5.

Figure 7 shows another circuit implementing mixing and RF switching functions for production of ultrawideband pulses, employing a combination of fixed gm amplifiers.
5   The circuit of Figure 7 combines independent input carrier signals via input metal oxide semiconductor field effect transistors (MOSFET transistors) 700 biased in their constant current regions to produce a tail current proportional to the weighted sum of inputs. The physical dimensions of the input MOSFET devices determine the gain or weighting of each device's input signal as represented in the summed output, which is gated by RF
10   output switch 701, and the size of the combining MOSFET 703 sets its gain. The combining transistor gain and the current drawn through current source 704 therefore determine the output signal level, in combination with the characteristics of the input MOSFETs. Each of inputs 1, 2, and 3 is either a carrier signal or a window function shaping signal component, and are combined and gated to produce RF output signal 702.
15   The capacitors coupled to each input serve as direct current blocking filters, such that any direct current bias on the input signal does not affect the biasing of the transistors in the circuit of Figure 7. Biasing each input transistor is handled by the resistor networks coupled to each input.

Figure 8 is a circuit diagram illustrating construction of an RF switch as is used to
20   gate the window-shaped carrier functions in Figures 4-7, and Figure 9 illustrates one embodiment of construction of such a circuit. While a single FET or other device may be used as an RF switch in some embodiments, the circuit of Figure 8 provides for gain, and better control of the output signal as is explained in greater detail below. The RF signal is input to the gate of p-type MOSFET M0, which is further coupled to a voltage source at
25   transistor M0's source and to the gate of n-type MOSFET M2 and drain of n-type transistor M1 at transistor M0's drain. A gating signal 802 is coupled to the gate of transistor M1, and transistor M1's source is connected to the drain of transistor M2 and to an output terminal 803. Transistor M3's source is connected to a ground or reference potential. This CMOS RF switch is operable to control the time duration and therefore the
30   spectral bandwidth of the output signal by controlling the width of the gating pulse input at 802, which allows current to flow from transistor M0 to M2.

An implementation of the RF switch circuit of Figure 8 is shown in cross-section form in Figure 9, which serves as an example of how such a circuit may be efficiently implemented in integrated circuit form. The RF input signal 801 is coupled to the gate of p-type MOSFET M0, and the gating signal 802 is applied to the gate of n-type MOSFET

5   M1. The gated output signal is provided from the coupled source of M1 and drain of n-type MOSFET M2. Power is applied by grounding the source of M2, while providing a power signal Vcc to the source of M0. The gate of M2 is further coupled to the drain of M1 and the drain of M0. In operation, the state of RF input signal 801 controls the state of output 803 when the gate signal 802 is at a logical high level, as all transistors operate in

10 saturation mode. The duration, and therefore the bandwidth, of the output signal 803 is controlled by the gating signal 802. In a further embodiment of the invention, the gating signal 802 is a clock signal, and the duty cycle of the clock signal is employed to control the duration and bandwidth of the output signal 803.

        Figure 10 illustrates an ultrawideband data communications system, consistent

15 with an embodiment of the present invention. A first signal source 1001 produces a window signal, which in some embodiments is derived from one or more sinusoidal signals as shown and discussed in conjunction with Figure 1. A carrier signal is produced by a second signal source such as second signal generator 1002, and is mixed with the window signal in mixer 1003 to produce a product signal such as that of Figures 2A and

20 2B. The output of the mixer is in some embodiments further gated by a radio frequency (RF) switch 1004 before coupling to an antenna 1005, while in other embodiments the RF switch is omitted and the output of the mixer is coupled to the antenna without an RF switch between. The antenna 1005 is operable to transmit or radiate a signal it receives and will take various forms in various embodiments of the invention, such as a Yagi

25 antenna configured to operate over a relatively wide frequency range.

        The output signal provided to antenna 1005 will be modulated with a data signal in further embodiments of the invention, such as via a mixer or switch coupled to receive the data signal and connected to one or more elements of the data communications system. For example, the data signal may be coupled to switch 1004, such that switch 1004 is used

30 to modulate the output of mixer 1003 with the data signal. Other embodiments include modulation of the window signal produced at 1001, modulation of the carrier signal produced at 1002, or modulation of the mixer 1003. Modulation of any of these

components can be implemented to result in modulation of the output signal sent to antenna 1005, and therefore modulate a signal radiated or transmitted from the antenna with the data signal.

These example embodiments of the present invention show how various circuit

5   elements can be constructed and employed to produce ultrawideband signals. Application of various window functions such as the sinusoidal functions given as examples here to a carrier signal result in ultrawideband pulses of controllable frequency and spectral width, making the present invention suitable for generation of ultrawideband pulses for communications applications. The present invention seeks in various embodiments to

10   apply analog window functions to an analog carrier signal to produce ultrawideband signals, as well as to produce of windowing functions using analog signals and processing as is demonstrated in these examples.

Specific embodiments have been illustrated and described herein, but it will be appreciated by those of ordinary skill in the art that any arrangement which is calculated to

15   achieve the same purpose may be substituted for the specific embodiments shown. This application is intended to cover any adaptations or variations of the invention. It is intended that this invention be limited only by the claims, and the full scope of equivalents thereof.

Claims

1. A method of generating an ultrawideband radio frequency pulse, comprising:

   generating a carrier signal having a selected frequency;

   shaping the carrier signal with a window function to produce an ultrawideband pulse.

5   2. The method of claim 1, wherein the window function comprises a sinusoidal function.

3. The method of claim 2, wherein the window function comprises one of a Hamming window, a Hanning window, and a Blackman window.

4. The method of claim 1, further comprising gating the shaped carrier to produce the ultrawideband pulse.

10   5. The method of claim 1, wherein the method is performed via a mixer and a CMOS radio frequency switch.

6. An ultrawideband radio frequency signal generator, comprising:

   a first signal generator operable to generate a sinusoidal window function;

   a second signal generator operable to generate a carrier signal; and

15   a mixer operable to produce an ultrawideband radio frequency product signal as a product of the sinusoidal window function and the carrier signal.

7. The ultrawideband radio frequency signal generator of claim 6, further comprising an RF switch operable to gate the ultrawideband radio frequency output signal.

8. The ultrawideband radio frequency signal generator of claim 7, wherein the RF switch

20   comprises a P-FET, a first N-FET and a second N-FET;

   the source of the P-FET coupled to the first voltage source, the gate of the P-FET coupled to the input voltage level, and the drain of the P-FET coupled to the drain of the first N-FET and the gate of the second N-FET;

the gate of the first N-FET coupled to receive the control signal, and the source of the first N-FET coupled to the drain of the second N-FET;

the source of the second N-FET coupled to the voltage reference.

9. The ultrawideband radio frequency signal generator of claim 6, wherein the mixer comprises a single-balanced mixer.

10. The ultrawideband radio frequency signal generator of claim 6, wherein the mixer comprises a double-balanced mixer.

11. The ultrawideband radio frequency signal generator of claim 6, wherein the mixer comprises a cascade of two or more fixed transconductance amplifiers.

12. An ultrawideband radio frequency data communications device, comprising:

a first signal generator operable to generate a sinusoidal window function;

a second signal generator operable to generate a carrier signal; and

a mixer operable to produce an ultrawideband radio frequency product signal as a product of the sinusoidal window function and the carrier signal.

13. The ultrawideband radio frequency data communications device of claim 12, further comprising an RF switch operable to gate the ultrawideband radio frequency output signal.

14. The ultrawideband radio frequency data communications device of claim 13, wherein the RF switch comprises a plurality of CMOS transistors.

15. The ultrawideband radio frequency data communications device of claim 12, wherein the mixer comprises a single-balanced mixer.

16. The ultrawideband radio frequency data communications device of claim 12, wherein the mixer comprises a double-balanced mixer.

17. The ultrawideband radio frequency data communications device of claim 12, wherein the mixer comprises a cascade of two or more fixed transconductance amplifiers.

18. A method of generating an ultrawideband radio frequency signal, comprising:
    generating a sinusoidal carrier signal having a selected frequency;
    generating a sinusoidal window shaping signal having a frequency lower than that of the carrier signal;
    mixing the carrier signal and window shaping signal to obtain a product signal; and
    gating the product signal to form an ultrawideband signal such that the window shaping signal component of the product forms a sinusoidal window pulse function.

19. The method of claim 18, wherein the sinusoidal window pulse function comprises one of a Hamming window, a Hanning window, and a Blackman window.

20. The method of claim 18, wherein the gating is performed via a CMOS radio frequency switch.

21. An ultrawideband radio frequency signal generator, comprising:
    a first signal generator operable to generate a sinusoidal window function;
    a second signal generator operable to generate a carrier signal; and
    a mixer operable to produce an ultrawideband radio frequency product signal as a product of the sinusoidal window function and the carrier signal; and
    an RF switch operable to gate the ultrawideband radio frequency product signal, wherein the RF switch comprises at least three coupled CMOS transistors.

22. The ultrawideband radio frequency signal generator of claim 21, wherein the at least three coupled CMOS transistor are coupled to a first voltage source, a voltage reference of a different voltage than the first voltage source, an input voltage level, a control signal, and an output conductor.

23. The ultrawideband radio frequency signal generator of claim 22, comprising a P-FET, a first N-FET and a second N-FET;

the source of the P-FET coupled to the first voltage source, the gate of the P-FET

coupled to the input voltage level, and the drain of the P-FET coupled to the drain of the

first N-FET and the gate of the second N-FET;

the gate of the first N-FET coupled to receive the control signal, and the source of

5   the first N-FET coupled to the drain of the second N-FET;

the source of the second N-FET coupled to the voltage reference.

24. The ultrawideband radio frequency signal generator of claim 22, wherein the voltage

reference comprises a ground voltage level.

25. An ultrawideband radio frequency data communications system, comprising:

10   a first signal generator operable to generate a sinusoidal window function;

a second signal generator operable to generate a carrier signal;

a mixer operable to produce an ultrawideband radio frequency product signal as a

product of the sinusoidal window function and the carrier signal;

a modulator that is coupled to receive a data signal from a data signal source,

15   the modulator further coupled to modulate the ultrawideband radio frequency product with

the data signal; and

an antenna coupled to receive the ultrawideband radio frequency product signal

and further operable to transmit the ultrawideband radio frequency product signal.


26. The ultrawideband radio frequency data communications system of claim 25, wherein

20   the modulator is coupled to the carrier signal produced by the second signal generator,

thereby operable to modulate the ultrawideband radio frequency product with the data

signal by modulating the carrier signal.

27. The ultrawideband radio frequency data communications system of claim 25, wherein

the modulator is coupled to the ultrawideband radio frequency product signal output from

25   the mixer, thereby operable to modulate the ultrawideband radio frequency product signal

with the data signal.

28. The ultrawideband radio frequency data communications system of claim 25, further comprising an RF switch coupled between the mixer and the antenna, thereby operable to gate the ultrawideband radio frequency product signal with the data signal.

29. The ultrawideband radio frequency data communications system of claim 28, wherein the mixer is coupled to the RF switch, thereby operable to modulate the ultrawideband radio frequency product signal with the data signal.

1/9
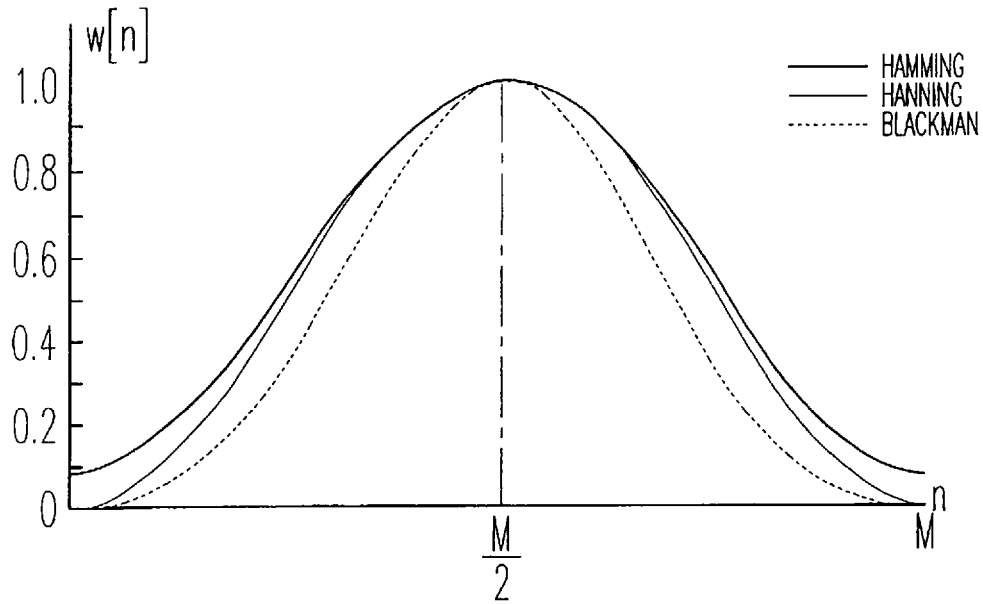
BLACKMAN
$$p(t)= \begin{cases} 0.42-0.5\cos(2\pi t/M) + 0.08\cos(4\pi t/M), & 0<t<M, \\ 0, & \text{otherwise} \end{cases}$$

HANNING
$$p(t)= \begin{cases} 0.5-0.5\cos(2\pi t/M), & 0<t<M, \\ 0, & \text{otherwise} \end{cases}$$
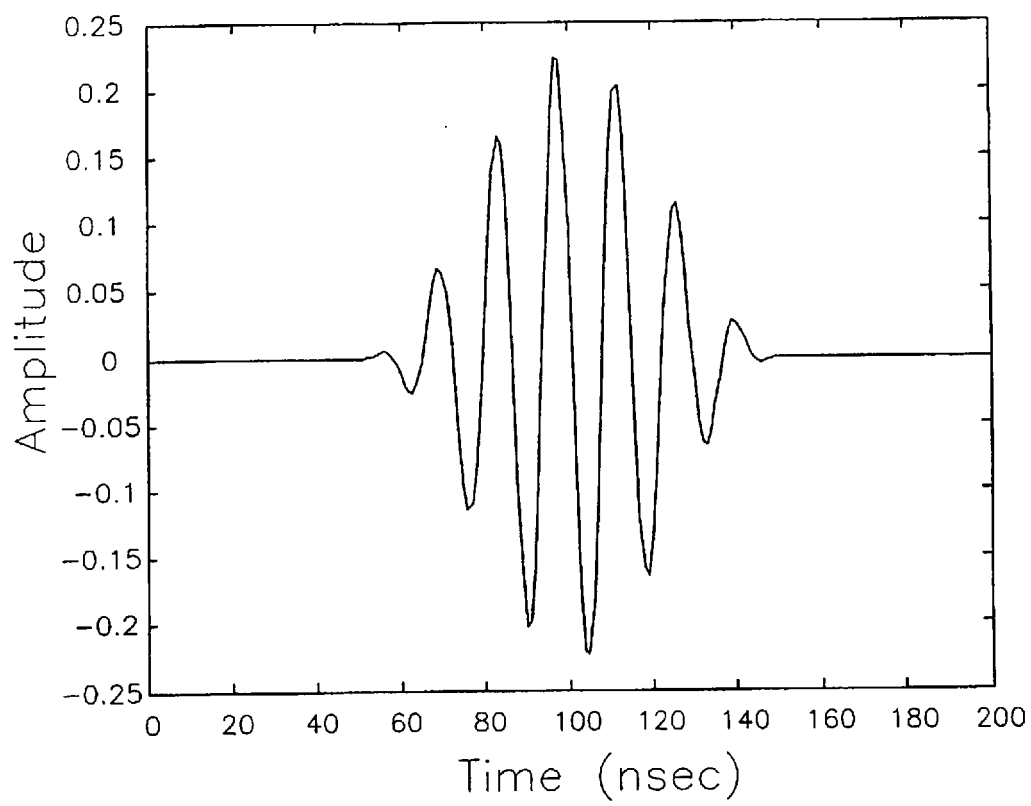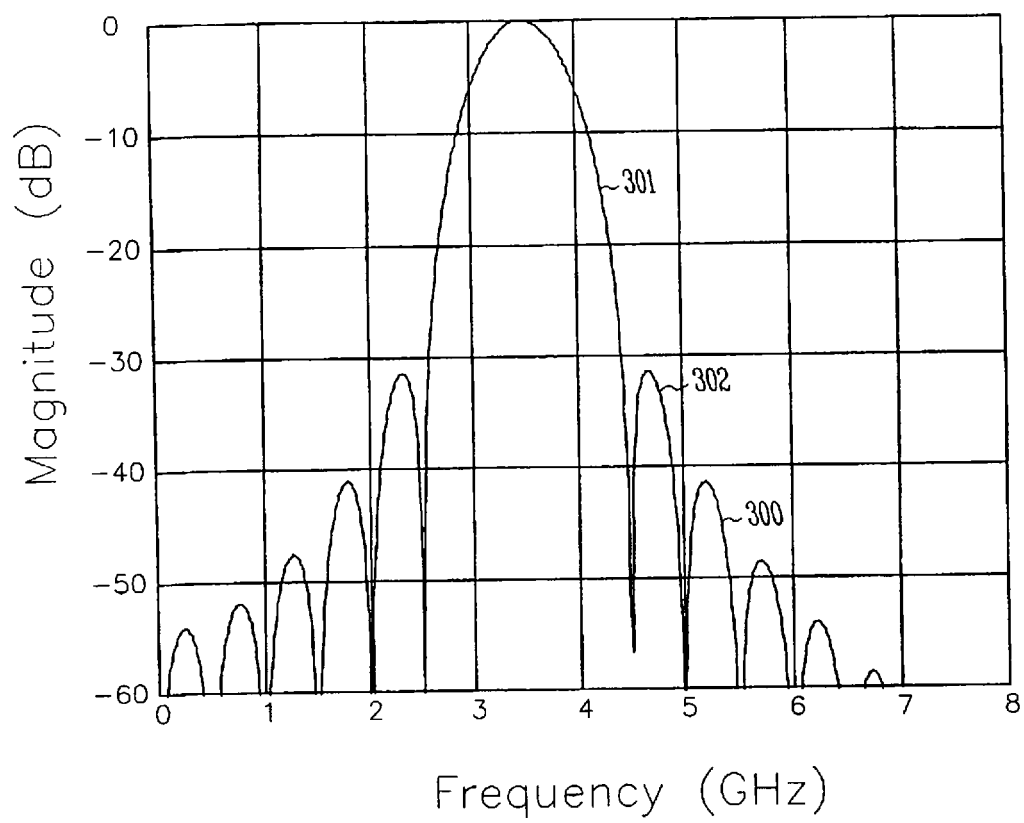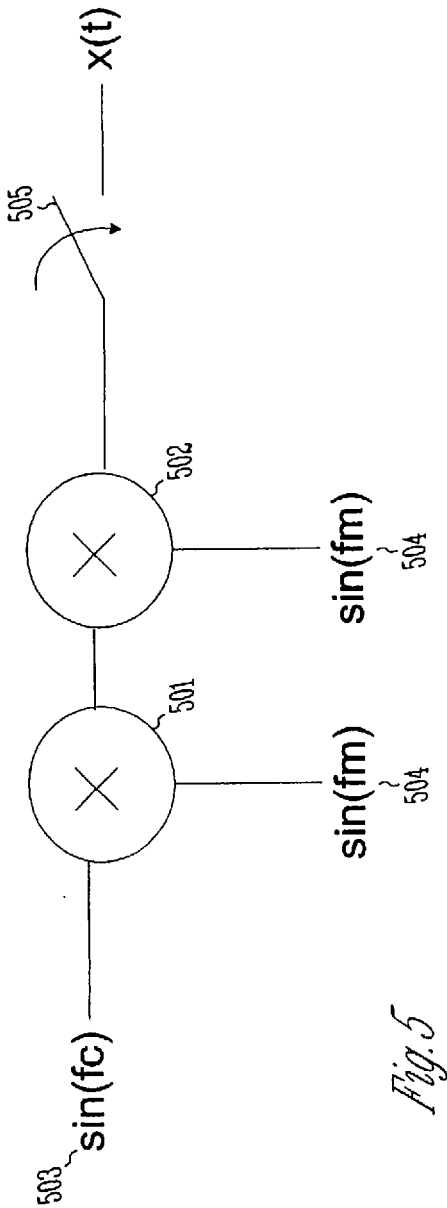
HAMMING
$$p(t)= \begin{cases} 0.54-0.46\cos(2\pi t/M), & 0<t<M, \\ 0, & \text{otherwise} \end{cases}$$

Fig. 1

2/9

Fig.2A

Fig.2B

Fig.3

Fig. 4

Fig. 5

Fig. 6

x(t)
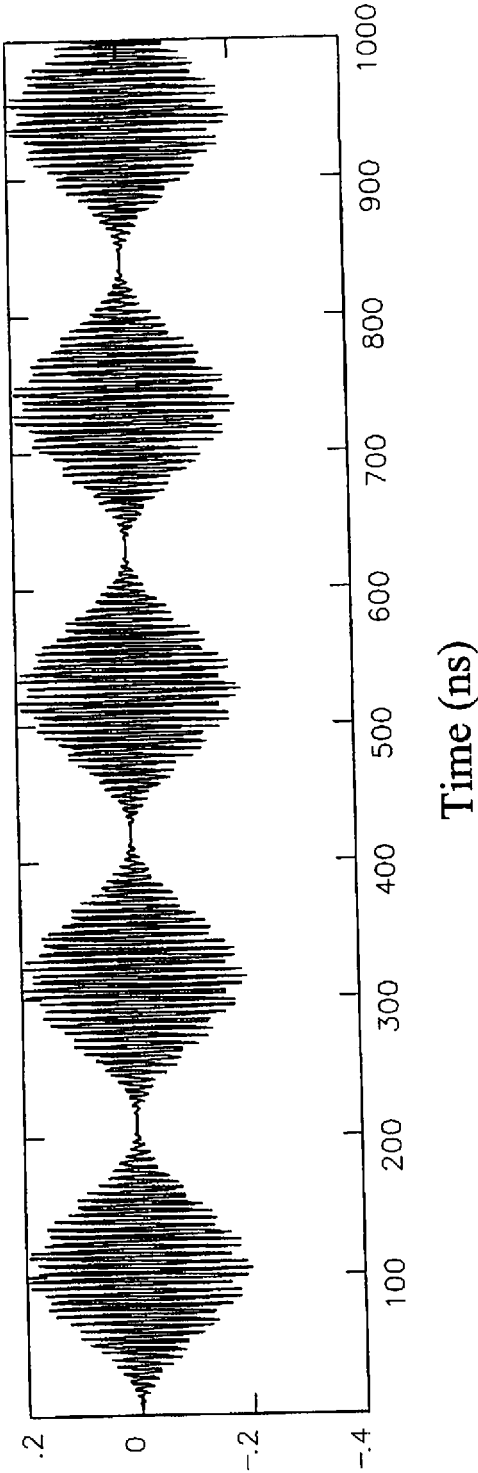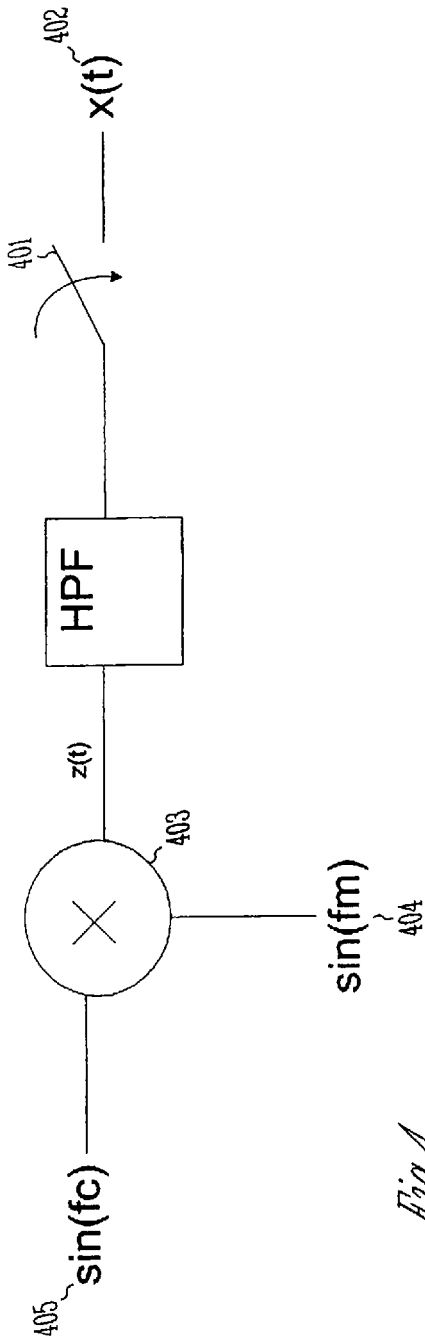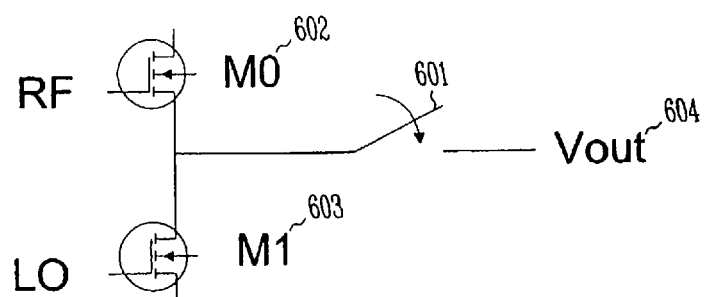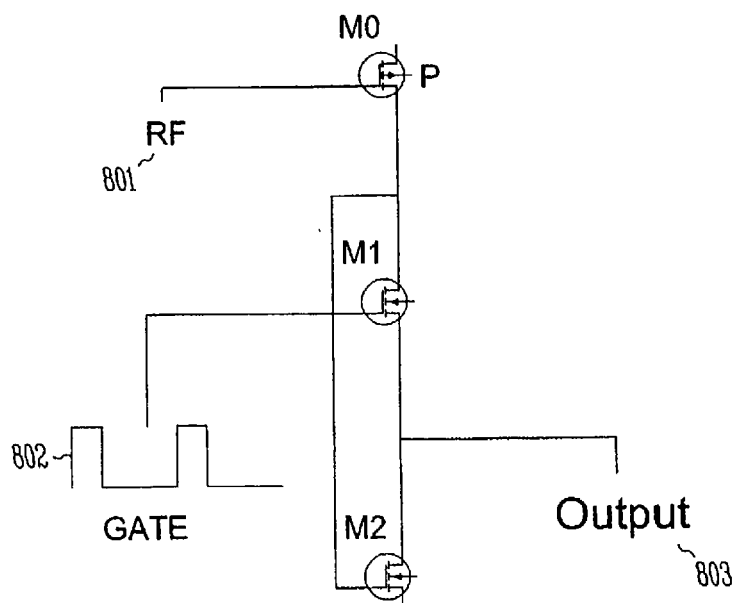
Fig. 8
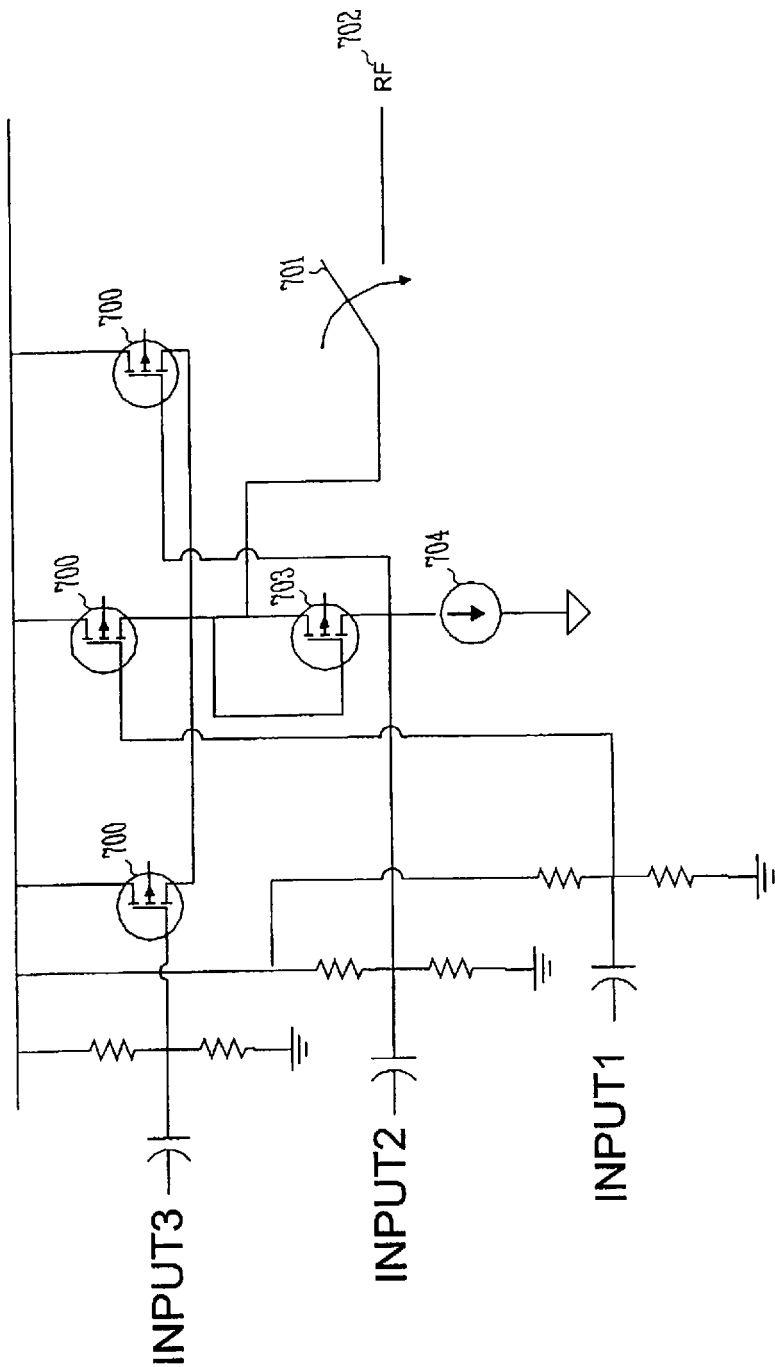
Fig. 7
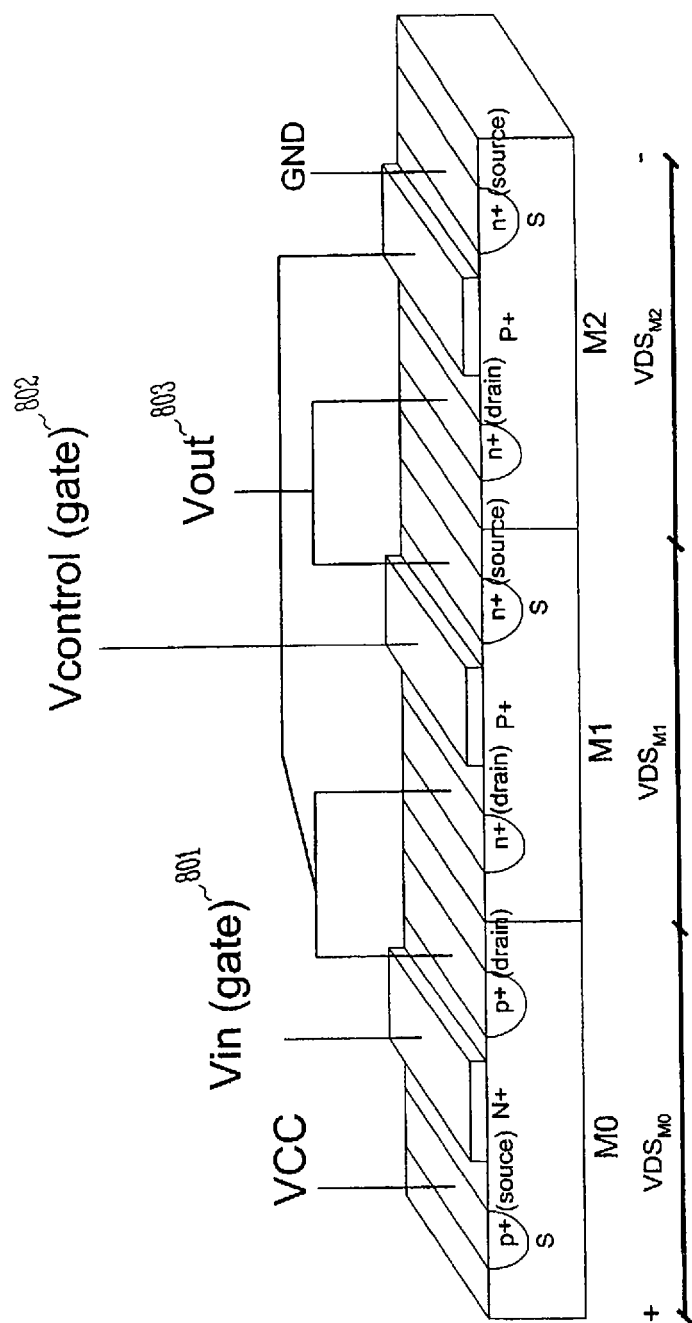
Fig.9

Fig. 10

INTERNATIONAL SEARCH REPORT

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7   H04B1/69   H03K17/04   H03D7/12

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7   H04B   H03K   H03D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, INSPEC, COMPENDEX, PAJ, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 01/39451 A (MULTISPECTRAL SOLUTIONS, INC) 31 May 2001 (2001-05-31)	1,4,5
Y	page 9, line 1 – page 10, line 28; figures 1,6	2,3,6, 9-12, 15-17, 25-27
	page 12, line 5 – line 21	
	page 13, line 3 – line 12	
	page 19, line 28 – page 20, line 13	

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[X] Further documents are listed in the continuation of box C   [X] Patent family members are listed in annex

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Date of the actual completion of the international search	Date of mailing of the international search report
22 June 2005	12/07/2005

Name and mailing address of the ISA	Authorized officer
European Patent Office, P.B. 5818 Patentlaan 2 NL – 2280 HV Rijswijk Tel. (+31–70) 340–2040, Tx. 31 651 epo nl, Fax. (+31–70) 340–3016	Giglietto, M

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INTERNATIONAL SEARCH REPORT

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No
X	ZHIQIANG WU ET AL: "High performance ultra-wide bandwidth systems via novel pulse shaping and frequency domain processing" 2002 IEEE CONFERENCE ON ULTRA WIDEBAND SYSTEMS AND TECHNOLOGIES 21-23 MAY 2002 BALTIMORE, MD, USA, 21 May 2002 (2002-05-21), pages 53-58, XP002332710 2002 IEEE Conference on Ultra Wideband Systems and Technologies (IEEE Cat. No.02EX580) IEEE Piscataway, NJ, USA ISBN: 0-7803-7496-7 paragraph '0002!; figure 4	1-5
Y	WO 01/93520 A (XTREMESPECTRUM, INC) 6 December 2001 (2001-12-06) page 11, line 14 - page 12, line 20	2,3,6, 12,25-27
Y	US 2003/052727 A1 (KOMURASAKI HIROSHI ET AL) 20 March 2003 (2003-03-20) figures 6,7	9-11, 15-17
P,X	ZIMMER R ET AL: "A simple method of generating UWB pulses" EIGHTH IEEE INTERNATIONAL SYMPOSIUM ON SPREAD SPECTRUM TECHNIQUES AND APPLICATIONS - PROGRAMME AND BOOK OF ABSTRACTS 30 AUG.-2 SEPT. 2004 SYDNEY, NSW, AUSTRALIA, 30 August 2004 (2004-08-30), pages 112-114, XP002332711 Eighth IEEE International Symposium on Spread Spectrum Techniques and Applications - Programme and Book of Abstracts (IEEE Cat. No.04TH8738) IEEE Piscataway, NJ, USA ISBN: 0-7803-8465-2	1-7, 12-14, 18-29
P,Y	the whole document	9-11, 15-17

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